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System design and operation for integrating variable renewable energy resources through a comprehensive characterization framework

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### 1 Abstract

2 The name itself – VRE for variable renewable energy – encapsulates the essential challenge: 3 these energy sources are attractive precisely because they are renewable and yet problematic 4 because they are variable. Thus, integrating large penetrations of VRE resources such as wind 5 and solar into the electricity grid will necessitate flexible technologies and strategies. This paper 6 establishes characterization metrics of both individual VRE resources and aggregated VRE 7 resource sets with the goal of quantifying the integration requirements of various typologies. 8 Integration requirements over multiple time scales are considered including hourly, weekly -9 seasonal, and inter-annual flexibility, as well as transmission expansion to connect neighboring 10 wind and solar sources, and demand response mechanisms. The respective integration 11 requirements are quantified through storage and demand response utilization rates, VRE curtailment rates, non-VRE ramping requirements, system costs, and GHG emissions. The results 12 13 from VRE resources across South America clearly quantify the impact that integrating different 14 VRE regimes has on the electricity system design and operation: not surprisingly integrating 15 VREs on a grid with low non-VRE flexibility incurs the largest integration requirements, while 16 smoothing net VRE production with out-of-phase resources is an effective integration strategy.

### 17 Keywords

- 19 Variable renewable energy integration
- 20 VRE Characterization
- 21 VRE flexibility resources
- 22 Electricity system dispatch model

### 23 **1 Introduction**

24 Among other things, the transition to a sustainable energy system depends on harnessing 25 renewable resources for electricity generation. Aside from hydro resources, the two most 26 important renewable resources, wind and solar, are variable in nature. The implications of 27 achieving large variable renewable energy (VRE) penetration in the electricity grid are not fully 28 quantified, nor the range of balancing options fully explored. In part, the particular 29 characteristics of a VRE regime impacts the specific combination of flexibility resources that are 30 required for its integration. As such, characterizing VRE regimes according to their integration 31 requirements is a critical step in the integration process, and is the primary subject of the 32 current paper.

33

34 As a preliminary example, consider that wind resources are often characterized using the 35 Weibull distribution, which describes windspeed distributions according to their annual mean windspeed and shape factor. While straightforward, the Weibull distribution is not a holistic 36 37 representation (Gunturu & Schlosser, 2012) (Jaramillo & Borja, 2004), and (Morrissey, Cook, & 38 Greene, 2010). Alternative characterizations provide a more nuanced view of VRE variability: 39 relationship between the mean and median wind power density (WPD), coefficient of variance, 40 robust coefficient of variance, inter-quartile range, inter-annual variation, consecutive hours 41 above or below a set WPD threshold (episode length), WPD availability above a given threshold, 42 and anticoincidence with the surrounding grid cells (Gunturu & Schlosser, 2012), (Cosseron, 43 Gunturu, & Schlosser, 2013), (Fant & Gunturu, 2013), and (Brower, Barton, Lledó, & Dubois, 2013). System-level analyses include the effective load carrying capability (Henson, McGowan, & 44 45 Manwell, 2012), the effect of temporally shifting a resource (Maddaloni, Rowe, & van Kooten, 46 2009) and the net load curve variability (Holttinen et al., 2010). The current work seeks to 47 closely tie wind characteristics to an overall system or VRE characterization for the grid.

48

49 In parallel to studies on specific resources, other studies have explored the impact of large-scale 50 VRE integration at a range of system scales. For example, a techno-economic analysis quantified 51 the impact of replacing conventional technologies with optimized hydrogen-based systems in 52 renewable-based stand-alone power systems (Zoulias & Lymberopoulos, 2007). Distribution 53 scale analyses have studied the impacts of high VRE penetration on distribution networks in 54 Lisbon and Helsinki (Paatero & Lund, 2007), and the Davarzan area in Iran (Valizadeh Haghi, 55 Tavakoli Bina, Golkar, & Moghaddas-Tafreshi, 2010). Transmission scale analyses have 56 quantified the integration of high wind, solar PV, and/or wave power in Austria (Burgholzer & 57 Auer, 2016), Central Queensland (Shafiullah, 2016), and Vancouver Island (Moazzen, Robertson, 58 Wild, Rowe, & Buckham, 2016), have identified the optimal mixtures of VREs to avoid excess 59 electricity production in Denmark (Lund, 2006), and have analyzed the desalination plants as a 60 deferrable load in Saudi Arabia (Al-Nory & El-Beltagy, 2014). Further studies have analyzed the 61 impact of VRE integration on specific non-VRE generation assets such as hydropower resources 62 and their associated river flow patterns (Kern, Patino-Echeverri, & Characklis, 2014), or thermal 63 power plant operational cycles (Göransson & Johnsson, 2009). Others have studied the impacts 64 of integrating renewable energy shares outlined in national policies in North-West Europe 65 (Deane, Driscoll, & Gallachóir, 2015), or the impact of storage size and efficiency on achieving 66 100% renewable systems (Weitemeyer, Kleinhans, Vogt, & Agert, 2015). Finally, a suite of 67 studies has quantified VRE integration economic costs through metrics such as increased need

for balancing services and flexible operation of thermal plants, and reduced utilization of capital
 embodied in thermal plants (Hirth, Ueckerdt, & Edenhofer, 2015).

70

71 This paper aims to bridge the gap between VRE characterization analyses and integration 72 requirements by presenting a new VRE resource characterization framework that maps VRE 73 characterizations to specific balancing strategies. VRE resources are characterized according to 74 their hourly, weekly, seasonal, and inter-annual temporal variability, as well as their geographic 75 coincidence factor, inter-resource coincidence factor, and correlation with the demand profile. 76 These metrics map to specific balancing strategies: storage technologies with daily or seasonal 77 reservoir capacity, VRE curtailment, increasing the non-VRE grid flexibility, interconnecting 78 geographically dispersed resources and VRE types, and demand response (DR) mechanisms. The 79 proposed characterization framework enables optimization of integration strategies for a given 80 suite of VRE projects. Although applied to a specific geographical area, the methodology 81 illustrated is general in scope. 82 83 The remainder of this paper is organized as follows: Section 2 first describes the VRE resource 84 data that were used in this analysis, while Section 3 details the six developed VRE 85 characterizations. Section 4 then quantifies the impacts of integrating VRE resource regimes 86 with distinct typologies in a production cost model. Finally, Section 5 discusses the overall

- 87 results and Section 6 presents our conclusions.
- 88

### 89 **2 VRE Resource Data**

90

Multi-decadal, continentally-scaled wind and solar PV generation timeseries with hourly 91 92 temporal resolution were produced using the Global Renewable Energy Timeseries and Analysis 93 (GRETA) tool (McPherson, Sotiropoulos-Michalakaos, Harvey, & Karney, 2017). GRETA applies 94 the Boland-Ridley-Lauret (Boland, Ridley, & Brown, 2008) and Perez (Perez, Seals, Ineichen, 95 Stewart, & Menicucci, 1987) models to NASA's MERRA radiation fluxes dataset to calculate 96 hourly solar PV generation, and the Archer and Jacobson Least Squares Fit (Archer & Jacobson, 97 2003) methodology to the MERRA atmospheric reanalysis dataset to calculate hourly wind 98 generation. The MERRA reanalysis dataset, developed by NASA (Rienecker et al., 2011) 99 (Lucchesi, 2012), aggregates weather observations from satellite and surface stations, aircrafts, 100 and balloons through a Numerical Weather Prediction (NWP) model (Brower et al., 2013). 101 Reanalysis datasets offer key advantages for creating the VRE resource estimates employed in 102 this analysis, including global coverage and long data collection periods (Boccard, 2009), and 103 consistent extrapolation methodology (Gunturu & Schlosser, 2012) (Brower et al., 2013). MERRA 104 provides the variables required to compute wind and solar generation potential on a global  $\frac{1}{2}^{\circ}$ 105 by 2/3 degree latitude-longitude grid with hourly resolution from early 1979 to within 2 months 106 of the present. GRETA has the same spatial and temporal resolution. The calculations assume a 107 100 m wind turbine hub height and use the Vestas-112-3.0 turbine power curve for wind 108 electricity, and assume fixed tilt solar panels with an elevation angle equal to the location's 109 latitude and use the First Solar FS395 power curve for solar electricity. 110

10 To illustrate the methodology, this analysis explores the VRE resource regimes available on the 112 South American continent. South America is chosen because it has high solar resource

113 availability in the Atacama Desert, Caribbean coast, and eastern Brazil, as well as excellent wind 114 resources in Patagonia, Paraguay, and Bolivia. Although country-specific VRE characterizations 115 analyses have been conducted in Brazil (Schmidt, Cancella, & Pereira Jr., 2016) and the Lerma 116 Valley in Argentina (Ramirez Camargo & Dorner, 2016), the entire South American continent, 117 including the regions listed above, has not yet been considered, to the author's knowledge. The 118 characterization analysis is limited to 'utility-quality' VRE regimes, defined as locations with an 119 average annual windspeed greater than 6.4 m/s, or an average annual solar irradiance greater 120 than 5.7 kWh/m<sup>2</sup>/day. Figure 1 highlights the grid cells that meet this criterion, using data from 121 the National Renewable Energy Laboratory (NREL, 2014) and (Gilman, Cowlin, & Heimiller, 122 2009). The characterization analysis was performed using more than 650 utility-quality cells over 123 35 years, resulting in almost 200 million data points. The following sections detail the 124 characterization framework developed to probe such a data set by quantifying balancing 125 requirements for distinct VRE regimes. The goal is to identify and highlight the most effective 126 balancing strategies. 127

128



129 130 131

Figure 1: Utility-quality solar PV (left) and wind (right) grid cells in South America that were selected for analysis

### 132 3 VRE Regime Characterization

A VRE regime's temporal variability, geographic correlations, and net load curve characteristics
 necessitate different integration technologies or strategies. Table 1 maps each VRE

135 characterization metric with the appropriate integration strategy. The suggested proposal is

- advanced as a candidate balancing strategy, a hypothesis which is subsequently tested using a
- 137 unit commitment model.

138	
139	Table 1: Resource variability metrics mapped to integration strategies

Characterization Metric	Metric Formulation	Corresponding integration strategy
Variability over	Hourly ramp events	Storage technologies with daily reservoir
hourly timescale	frequency and magnitude	capacity, VRE curtailment, and increasing
	(Eq. 1)	the non-VRE grid flexibility factor
Variability over	Relative frequency	Storage technologies with annual reservoir
weekly-seasonal	distribution curve (Eq. 2)	capacity, and increasing the system's firm
timescale		capacity
Inter-annual	Annual average capacity	Long-term storage technologies, sector
variability	factor distribution (Eq. 3)	integration, and backup generation
Correlation with	Average resource within	Demand response initiatives
demand profile	low or high demand	
	portions of the day (Eq. 4)	
Geographic	Coincidence of an	Transmission capacity expansion with
coincidence factor	increasingly large	neighboring areas
	geographic area (Eq. 5)	
Inter-resource	Correlation between wind	The respective share of wind versus solar
coincidence factor	and solar resources (Eq. 6)	resources

140

141 Each of the following metrics is first formulated and then applied over 650 South American grid

- 142 points according to 35 years (1979-2013) of historical meteorological data. For simplicity of
- 143 notation, sums over the whole data set are reduced from  $\sum_{1979}^{2013}$  to the form  $\sum_{a}$ . A number of
- 144 metrics are used to more comprehensively characterized each VRE resource.

### 145 **3.1 Hourly Variability**

146Ramp events are calculated by the rate of change in wind speed magnitude, as measured in147meters per second, between consecutive hours, thus resulting in units of  $[\frac{m}{s}]/h$ . We define the148mean absolute ramp rate ( $E_{MARV}$ ), between consecutive hours over the 35-year period as:149Eq. 1

150 
$$E_{MARV} = \frac{\sum |v_i - v_{i-1}|}{n-1}$$

151

152 where  $v_i$  refers to the wind speed in the hour *i*, and *n* is the number of hours over the 35-year 153 sequence. The mean absolute ramp rate for each grid point was calculated, then three 154 categories are defined at the 33 and 67 percentile values, such that each category contains one 155 third of the grid points. The cut-offs for the mean absolute ramp categories were calculated to 156 be 0.41 m/s per hour and 0.45 m/s per hour for the wind resource, and 76 W/m<sup>2</sup> and 83 W/m<sup>2</sup> 157 per hour for the solar resource. Figure 2 shows an example of a low, moderate and high hourly 158 variability wind resource over one year.





#### 3.2 Weekly-seasonal Variability 177

Weekly-seasonal variability is quantified by a regime's relative frequency. The maximum relative 178 179 frequency  $(E_{MRF})$  formulation for a wind resource is: Eq. 2

180

$$181 \qquad E_{MRF} = \frac{\max_{0 < i \le 23} y}{n}$$

182

183

where  $y_i$  is the number of samples within bin *i*, with bins spanning the range from 0 to 23 m/s 184

in  $1 \frac{m}{s}$  intervals, and *n* represents the total number of samples (hours) over the 35-year period. 185

186 Resources with high maximum relative frequency are consistently found within a specific

187 resource bin (not necessarily the largest bin) and have a narrow relative frequency distribution,

188 requiring less balancing for integration. Conversely, regimes with a small maximum relative

189 frequency and a broad relative frequency distribution require more non-VRE flexibility for

- 190 integration. Examples of wind regimes with low, medium, and high seasonal variability are 191 shown in Figure 5.
- 192 193





Figure 5: Relative frequency of windspeeds with low, average, and high seasonal variability

The maximum relative frequency is correlated with the average windspeed: lower average
windspeed grid points tend to have a higher maximum relative frequency and vice versa (Figure
6). This is intuitive: regimes with low average windspeed are consistently weak, resulting in a
higher maximum relative frequency, while high average windspeed grid points have a larger
windspeed spread and lower maximum frequencies. From year to year the relative frequency
distribution varies more for regimes with higher overall maximum relative frequency.





Figure 6: Relationship between the maximum relative frequency and average windspeed

In general, solar resources have a wider relative frequency distribution and smaller maximum
relative frequency than wind resources: solar points clearly fluctuate from zero to (near) peak
levels on a daily basis. The variability among different solar resources is also narrower as shown
in Figure 7. Like wind, grid points with larger average irradiance have smaller maximum relative
frequency, although to a lesser extent than wind.



209 210

211

Figure 7: Relationship between the maximum relative frequency and the average solar irradiance

### 212 3.3 Inter-annual Variability

213Inter-annual variability is calculated by determining the variance between the annual average214resource and the 35-year average resource. The inter-annual variance ( $E_{IAV}$ ) formulation is:215Eq. 3

$$E_{IAV} = \frac{\sum_{n=1}^{35} (y_i - \mu)^2}{35}$$

217

216

where  $y_i$  is the is the average resource value in year *i*, and  $\mu$  is the 35-year average. Three interannual variability categories are defined with boundaries at variances of 0.12 and 0.19 (m/s)<sup>2</sup> per year for wind, and at 5.8 and 35 (W/m<sup>2</sup>)<sup>2</sup> per year for solar; each category contains one third of the points.

222

The most variable wind grid point has average inter-annual variation of 10%, and a maximum annual variation of 22%; however, over 70% of points have a 35-year average inter-annual variation less than 4%. Overall, solar resources experience a smaller range in inter-annual variation than wind. The most variable solar grid point has an average inter-annual variation of 5%, less than half the respective value for the wind resource.

228

The inter-annual variance is closely related to the interquartile range, as shown for the wind grid points in Figure 8. Wind grid point's interquartile range spans from 0.19 to 1.10 m/s while the variance ranges from 0.02 to 0.56 (m/s)<sup>2</sup> per year.



232 233

Figure 8: Relationship between variance and interquartile range for the wind grid points



### 235 3.4 Correlation with demand profile

 $E_{DR} = y_1 + 2y_2 + 3y_3 + 4y_4$ 

236 Demand response (DR) can at least partly shift the load profile to match the available VRE 237 resource. DR's utility is informed by the correlation between the VRE resource and the demand 238 profile. A characteristic demand profile was approximated by allocating each hour in the day to 239 one of four demand blocks, ranging from low demand hours in block 1 to high demand hours in 240 block 4. The approximated demand profile is built from publicly available historical Chilean 241 demand data (including all consumer categories) from the Chilean electricity system regulator 242 (Coordinador Electrico Nacional, 2015) (Central Energia, 2015). The DR metric is formulated by 243 averaging the resource within each block, normalizing to the 35-year average, and summing 244 over the four DR blocks to produce the aggregate DR metric. The DR metric  $(E_{DR})$  formulation is 245 calculated as follows:

246

Eq. 4

247

248 249 where  $y_1, ..., y_4$  is the average resource value (m/s or W/m<sup>2</sup>) observed in the respective demand 250 block 1, ..., 4 (as defined by the demand profile shown in Figure 9). For example,  $y_1$  is the 251 average resource value for the hours in the day which fall into demand block 1. Resources 252 during demand block 2 carry twice as much weight as resources during demand block 1 (from a 253 demand-matching perspective), because the average demand in block 2 is twice that in block 1, 254 after subtracting the minimum demand; similarly for the weighting factors of 3 and 4 for resource values during demand blocks 3 and 4. Figure 9 shows the variation with hour of day in 255 256 wind speed and the demand profile, averaged over 35 years of hourly data, for two example grid 257 points, one with a low correlation between wind and demand, and the other with a high 258 correlation. 259



262

Figure 9: The DR block number plotted against the 24-hour average windspeed for well-263 correlated and anti-correlated wind regime; note the correlation (r) and DR metric value ( $E_DR$ ) 264 shown in the legend

Figure 10 demonstrates how the aggregated DR metric for wind varies among the grid points. 265 266 Only 30% of points have a higher average windspeed in low demand hours as compared to their 267 overall average. The DR metric variation is larger for lower average windspeed points, ranging by 268 over 5%, compared to only 2% for points with higher average windspeeds.



269 270

271 Figure 10: Relationship between the aggregate DR metric and the 35-year average windspeed

272 Predictably, all solar points have higher average irradiances in high demand hours, resulting in 273 an average  $E_{DR}$  of 3.55 across all grid points. There is a positive correlation (r = 0.576) between 274 the  $E_{DR}$  and the average irradiance: high average irradiance points have a proportionally higher irradiance in high demand hours, as compared to their low average irradiance counterpart 275 276 (Figure 11).





279

## irradiance

#### 280 3.5 **Geographic coincidence factor**

281 The geographic coincidence factor measures the correlation among neighboring areas' regimes, 282 to inform the benefit of transmission interconnection. The continuous geographic coincidence 283 factor  $(E_{CF})$  formulation is computed as: 284

Eq. 5

$$E_{CF} = \frac{\max_{1 \le h \le 24} \{\sum_{n=1}^{N} \widehat{y_{n,h}}\}}{\sum_{h=1}^{24} (\max_{1 \le n \le N} \widehat{y_{n,h}})}$$

286

285

where  $\hat{y}_{n,h}$  is the mean resource magnitude at location n, for a given hour h of each day. The 287 288 following simple example, comparing well-correlated and anti-correlated wind pairs over one 289 day, illustrates the geographic coincidence factor.



295 The windspeed timeseries in Figure 12 have geographic coincidence factors of 0.13 and 0.087 296 for the well-correlated and anti-correlated pairs, respectively. This simple example compares 297 only two grid points in a single day; however, practical applications calculate the geographic 298 coincidence factor for a given set of N points using the mean resource over multiple years; thus, 299 this simple example results in high geographic coincidence factors than more aggregated 300 practical applications. The geographic coincidence factor is low for non-coincident sets (e.g. 301 0.035 for a group of 10 points in the Patagonia Group 1 set), and high for coincident sets (e.g. 302 0.045 for a group of 10 cells in the Bolivia Group 4 set). The geographic coincidence factor 303 decreases for increasingly large groups of grid points; for example, the geographic coincidence 304 factor decreases from 0.05 for two grid cells to 0.035 for 50 grid cells in an example set in 305 Bolivia. However, the rate of change depends on the points included in the set, as shown in 306 Figure 13. 307

Wind's geographic coincidence factors changes depending on the area of the set of points under
 consideration: increasing cluster sizes from 2 to 50 induces a smaller change in geographic
 coincidence factor in Patagonia (average of -0.0104) as compared to Bolivia (average of -

- 311 0.0129), as shown in Figure 13.
- 312



313

314 Figure 13: Geographic coincidence factor for clusters of different sizes in Patagonia and Bolivia

315 Predictably, solar tends to have a higher coincidence factor than wind for the same sized set of

points: wind's coincidence factor depends on the choice of specific points, whereas solar's

317 coincidence factor depends on its location.

### 318 **3.6** Inter-resource coincidence factor

The inter-resource correlation factor ( $E_{IRC}$ ) informs the value of interconnecting wind and solar regimes by comparing the 35-year averaged wind and solar resource for each hour in a given

Eq. 6

321 day, as formulated in the following way:

322

323 
$$E_{IRC} = \sum_{n=1}^{24} \chi_n$$

324 where,

325  
326 
$$\chi_n = \begin{cases} 1 & \psi_{n,w} = \psi_{n,s} \\ 0 & \psi_{n,w} \neq \psi_{n,s} \end{cases}$$

327

328 
$$\psi_n = \begin{cases} 1 & y_n > \overline{y_n} \\ -1 & otherwise \end{cases}$$

and  $\overline{y_n}$  is the daily-averaged resource,  $y_n$  refers to either  $y_{n,w}$  (wind) or  $y_{n,s}$  (solar) resource in hour n, and  $n \in \{1, 2, 3, ..., 24\}$  hours in the day. Combinations with low aggregated interresource coincidence factors represent wind and solar point pairs that frequently have opposite variations (Figure 14**Error! Reference source not found.**); these resources would benefit from interconnection. By contrast, resources with similar hourly profiles (Figure 15), would benefit less from such interconnections.







Figure 14: 35-year averaged windspeed and solar irradiance for two anti-correlated nearby sites





Figure 15: 35-year averaged windspeed and solar irradiance for two well-correlated nearby sites

340

341	The examples in Figure 14 and Figure 15 have correlations of 0.814 and -0.929, and inter-
342	resource coincidence factors of 22 and 1 for the well correlated and anti-correlated pairs,
343	respectively. Only 20% of wind grid points have different tendencies compared to the average
344	than their solar counterpart in the same hour, implying a limited rationale for wind-solar
345	interconnections within the majority of selected points in South America.

### 346 3.7 Relationships among individual characterization metrics

An aggregated view that incorporates each characterization metric is desirable for understanding the relative advantage of different balancing strategies for a specific point. There is a wide range of variability characterizations for wind regimes across South America: of the 54 possible combinations of individual metrics including three hourly, weekly-seasonal and inter-

- 351 annual variability categories each, as well as two DR/solar correlation categories, 51 were
- 352 represented by at least one grid point. Note that for simplicity, the DR and wind-solar
- 353 correlation metrics are reduced to one, since the demand profile mirrors the solar profile, as
- shown by the DR metric in Figure 11. Figure 16 shows five examples of such individual variability
- 355 combinations, spanning from the least to most intensive integration requirements.



The 'low-variability' cumulative category (representing 16 grid points) scores one in the four individual variability categories, while the 'high-variability' cumulative category (representing 4 grid points) scores two or three in the four individual variability categories. In between, the lowmedium variability represents 10 points, medium variability represents 17 points, and mediumhigh variability represents 23 points. The nine most prevalent cumulative categories represent approximately half of the selected South American wind grid points, shown in Table 2.

Table 2: Definition of wind types according to variability characterization metrics

Wind Type:	Α	В	С	D	Е	F	G	Н	I
Proportion of South American cells	9%	8%	4%	6%	4%	4%	4%	4%	6%
Hourly variability	Х	*	Х	*	*	-	-	-	-
Weekly/seasonal variability	*	Х	*	Х	Х	*	-	-	-
Inter-annual variability	-	Х	*	*	-	Х	Х	*	-
Correlation with demand or solar profile	Х	-	-	-	-	-	-	-	-

In Table 2, the symbol 'X' is used to represent high balancing requirements, whereas '\*' 368 369 represents moderate balancing requirements, and '-' represents low balancing requirements. 370 Wind types A and B are the most and prevalent and demanding because both require a high 371 level of two integration strategies: high hourly variability and anti-correlation with demand or 372 high weekly-seasonal and inter-annual variability, respectively. Wind type A is the only prevalent 373 category that includes deployment of demand response or interconnection with solar sites as an 374 effective balancing strategy, as expected by the relatively small number of grid points that were 375 negatively correlated with the demand or solar profile. Conversely, wind types C-G require a 376 high level of only one balancing strategy, and wind types H-I are the least demanding types to 377 integrate, since they do not require a high level of any balancing strategy. 378 379 There is a strong correlation between weekly-seasonal variability and hourly variability, and 380 between weekly/seasonal variability and inter-annual variability. Compared to wind, solar 381 resources are more variable hourly, but less variable inter-annually. Solar resources also

- 382 correlate much more with demand, decreasing the incentive for demand response initiatives.
- 383 Solar has a much higher coincidence factor for the same group of points, decreasing the utility
- 384 of transmission interconnection.

#### Modelling VRE typologies to quantify integration 4 385

#### requirements 386

387 A unit commitment (UC) model is developed to quantify the balancing requirements associated 388 with integrating different VRE typologies. The UC model minimizes the system costs over a 389 defined optimization period, while abiding by a list of operational constraints, including: system-390 wide load-power balance; power limits, ramping limits, and minimum up/downs (generator, 391 storage, and DR assets), energy limits (storage assets only), daily utilization balance (DR assets 392 only). The UC algorithm is built on the minpower repository (Greenhall, Christie, & Watson, 393 2012), with several modifications to include representations of demand response and storage 394 assets, and differing integration system parameterizations. Storage technology operation is 395 limited by additional constraints, including either pumping or generating in a given hour, and 396 minimum and maximum energy storage constraints (e.g. the reservoir level in the case of a pumped hydro storage unit). Demand response is constrained by absolute and relative (as a 397 398 percentage of scheduled load) limitations on an hourly and daily basis. A series of scenarios was 399 devised to test different integration strategies; all scenarios share the following assumptions: 400

- Simulation over a full year using 2012 meteorological data, •
- 401 • Characteristic demand profile, with either hourly or weekly temporal resolution,
- 402 Hydro power limitations according to historical daily flow data, published by the Chilean • electricity system regulator (Coordinador Electrico Nacional, 2015) (Central Energia, 403 404 2015),
- 405 • Generator cost (Table 3) and operational limitations (Table 4),
  - Storage asset cost (Table 5) and characteristics (Table 6), ٠
- 407 VRE assets are sized such that 60% of total generation could be supplied by VRE • 408 resources prior to curtailment,
- 409 All scenarios are normalized to have the same available VRE generation prior to • 410 curtailment.
- 411

- Table 3: Generator technology costs: total overnight cost [2012 USD/kW] from Table 8.2 of (U.S.
- 413 Energy Information Administration, 2014a), fixed and variable O&M and fuel [2012 USD/MWh]
- 414 from Table 1 of (U.S. Energy Information Administration, 2014b) and GHG emissions from Table

415 A.111.2 of (Schlomer et al., 2014) and (Black & Vetch Holding Company, 2012)

Technology	Total overnight cost	Capacity factor	Fixed O&M cost	Variable O&M plus fuel	GHG emissions
	[\$/kW]	[%]	[\$/MWh]	[\$/MWh]	[gCO2eq/kWh]
Hydro	2,435	53%	4.1	6.4	24
Natural Gas (CC)	915	87%	1.7	49.1	490
Natural Gas (simple)	971	30%	2.8	82.0	490
Biomass	3,919	83%	14.5	39.5	230
Wind (onshore)	2,205	35%	13.0	0	11
Solar PV (utility)	3,564	25%	11.4	0	48

416 417

Table 4: Generator operating constraints by technology

Generator Type	Minimum Load	Cold Start	Spinning Ramp	Minimum off time	Start-up cost	Operating coefficient
/1= =			Rate			***[% of
	[%] <sup>[1]</sup>	[hours]	[%/min] <sup>[1]</sup>	[hours] <sup>[2]</sup>	[\$/MW] <sup>[2] *</sup>	generation]
Natural Gas	50%	0.4 <sup>[3]</sup>	8.3	0	26	42%
(simple)						
Natural Gas	50%	3.5 <sup>[3]</sup>	5	2	66	33%
(CC)						
Coal /	40%	<b>3</b> <sup>[3]</sup>	2	8	54	33%
Biomass **						

418 References for Table 4: [1]: (Black & Vetch Holding Company, 2012); [2]: (Schill, Pahle, &
419 Gambardella, 2016); [3]: (Parsons Brinckerhoff, 2014)

419 Gambardella, 2016); [3]: (Parsons Brinckernon, 2014)

420 \* Euros were converted to US dollars with the average 2015 EUR/USD exchange rate of 1.11

- 421 \*\* Assuming coal to biomass conversion
- 422 \*\*\* Describes the flexibility associated with each generation category
- 423
- 424 Table 5: Storage technology cost data (Luo, Wang, Dooner, & Clarke, 2014)-Table 12.

Technology	Power Capital Cost [\$/kW]	Energy Capital Cost [\$/kWh]	Cycle Efficiency [%]
Pumped hydro	3000	12	80%
storage			
Hydrogen fuel cell	2300	15	50%

426

Table 6: Storage technology properties (Luo et al. 2014, Figure 16 & Table 12)

Storage Technology	Applicable power system size range	Applicable energy capacity	Typical storage duration	Cycle Efficiency	Discharge time at power rating
Pumped hydro	2 GW	48 GWh	Hours-days	85%	Hours
storage					
Hydrogen	50 MW	36 GWh	Days-months	55%	Days
electrolysis and storage					

427

### 428 4.1 The impact of hourly variability on integration requirements

429 The impact of hourly variability on integration requirements is tested through three scenarios: a 430 baseline scenario with an average non-VRE flexibility factor grid and no VRE curtailment costs, 431 systems with either high or low flexibility factors, and a system that incurs VRE curtailment 432 costs. The flexibility factor represents the system's capacity to respond to variation in the net 433 load curve and depends on the installed capacity by generation type, where each generation 434 technology has distinct flexibility parameters (operating, ramping, and minimum downtime). 435 The flexibility factor is discussed in more detail in Section 4.1.2. The scenarios have a 168-hour 436 optimization period, and exclude demand response and seasonal storage, which are scheduled

437 at the daily or annual planning horizon.

### 438 4.1.1 Impact on a system with an average flexibility factor and no curtailment costs

439 The baseline scenarios assume an average non-VRE flexibility factor, represented by 55% hydro,

440 32% simple cycle natural gas, 8% combined cycle natural gas, 3% biomass, and 3% coal. The

impact of hourly resource variability on system integration is quantified in terms of storage

442 utilization rates, VRE curtailment rates, non-VRE ramping events, average system marginal cost,

variability in marginal system cost, and GHG emissions. The system's deployment for an example

444 week in the year is shown in Figure 17.



wind resource (top) versus a steady wind resource (bottom)

449 Integrating a variable wind resource requires both a larger storage reservoir capacity, as shown

450 in Figure 18, as well as larger and more frequent storage ramping cycles compared to the steady

451 wind resource.



452 453 454

Figure 18: Storage utilization as demonstrated by the energy stored in each hour for a system integrating a highly variable wind versus a steady wind resource

455 Accounting for the entire year, integrating an hourly-variable wind resource results in an 82% increase in storage required, 48% increase in non-VRE or storage ramping events, and 61% 456

increase in GHG emissions over an hourly-steady resource. Additionally, integrating a variable
resource results in a 52% increase in average system marginal cost and a 118% increase in
marginal cost variability (in terms of hourly spot market price). More significantly, integrating an
hourly-variable resource results in a 330% increase in wind generation curtailment over an

- 461 hourly-steady resource.
- 462

### 463 4.1.2 Impact on a system with a high and low flexibility factor

In addition to the VRE regime's nature, the integration requirements depend on the gridconfiguration characteristics. The following two scenarios explore the impact of the non-VRE

- 466 flexibility on integration requirements by comparing three grid configurations, each with the
- 467 same VRE regime and storage capacity but different non-VRE capacities (as shown in Figure 19).
- 468



469 Figure 19: Installed capacity on a system with a low (left), average (middle), and high (right)
 470 flexibility factors

The system's flexibility factor is quantified by its operating, ramping, and minimum downtime
flexibilities. The operating flexibility describes the flexibility of the assets dispatched in each

473 scenario, and is a product of the operating coefficient by technology (detailed in Table 4) and

the share of generation from each technology. The ramping flexibility describes the capacity of

- the system to adjust on an hourly basis, and is quantified by the product of the ramp rate (in
  MW/h per MW<sub>capacity</sub>) by technology (detailed in Table 4) and the installed capacity by
- 477 technology. The minimum downtime flexibility describes the frequency with which generation
- 478 assets can be turned off and on and is quantified by the product of the minimum downtime (in
- 479 hours) by technology (detailed in Table 4) and the installed capacity by technology. The relative
- 480 flexibilities for each scenario, ranked against the inflexible system, are show in Figure 20.



481



Figure 20: System operating flexibility, ramping coefficient, and minimum downtime coefficient for three scenarios with a low, average, and high flexibility factors

484 As demonstrated in an example week (Figure 21) the combined cycle natural gas plants in the 485 inflexible system are almost always on, even if they are at their minimum load, due to their 486 relatively long minimum down times and expensive startup costs. This leads to a number of 487 outcomes, including an increase of more than 300% in GHG intensity and in average system 488 marginal cost, as well as a 125% increase in curtailment over a flexible system. Storage 489 utilization, interestingly, is 10% higher in a flexible system, since the relatively fast spinning 490 ramping rates of NG combined cycle plants provide ramping capacity in the inflexible system. On 491 the other hand, utilizing the storage unit in the flexible system can avoid starting the natural gas 492 startup and incurring the associated startup and operating costs. 493



498

499 500 Figure 21: Generation by technology type for a system with a low (top), average (middle), and high (bottom) flexibility factor, when integrating a variable wind resource

### 501 4.1.3 Impact on a system that incurs curtailment costs

502 In a system that incurs 10 \$/MWh curtailment charges with a variable wind resource, the

curtailment decreases by 22%, while the storage increases by 3%, and GHG emissions increases
by 39% over a system that does not charge curtailment costs.

### 505 4.2 The impact of seasonal variability on integration requirements

506 A seasonally variable wind regime generates well-above or below average demand for

- significant portions of the year, resulting in larger negative and positive net load extreme values.
- 508 On the other hand, the seasonally steady regime generates more consistently throughout the
- 509 year, matching average demand and resulting in smaller negative and positive net load

- 510 extremes. The net load curves (electricity demand minus available VRE generation) in Figure 22
- 511 and Figure 23 are quantile functions, which show the number of weeks in the year for which the 512 net load is less than the corresponding value given on the vertical axis.





The VRE curtailment resulting from negative net loads in a system integrating a seasonally
 variable regime can only be mitigated with seasonal storage. As a result, integrating a seasonally

517 variable wind regime results in a 410% increase in storage asset utilization and a 211% increase

in storage energy capacity compared to its seasonally steady counterpart. Figure 23 shows the

519 respective net load curves including storage deployment.





Figure 23: Net load curve of a seasonally variable and steady resource with storage utilization

Two scenarios with averaged 52-week optimization periods were developed to test the effect of seasonal variability on integration costs; these scenarios exclude daily storage and demand response, but include seasonal storage. By deploying seasonal storage with a seasonally variable resource, the VRE curtailment is reduced to 1,400 MWh or 1% of the available VRE generation, which is the result of inflexible non-VRE generators, rather than negative net load. Additionally, seasonal storage deployment reduces curtailment by over 500%, average system costs by 10%, GHG emissions by 11%, and non-VRE and storage ramping events by 9%.

529

Integrating a seasonally variable resource results in a 6% increase in overall system costs and
GHG emissions, and 26% increase in non-VRE or storage ramping events compared to its
seasonally steady counterpart. The storage unit in both scenarios has a net accumulation of 2
GW annually, which could be used in the heating or transport industries. The weekly averaged
dispatch by generation type for a system with a seasonally steady versus seasonally variable
resources is shown in Figure 24.



(top) versus a seasonally variable resource (bottom)

#### 4.3 Integrating VRE resources that correlate with the demand profile 540

541 A wind regime that is well-correlated with the demand profile will be strong during high demand 542 hours resulting in smaller positive net loads, and weak during low demand hours resulting in 543 smaller negative net loads. In this case, demand response, which shifts the demand profile to 544 better align with the VRE resource, would be less attractive than its anti-correlated counterpart. Examples of the resulting net load curve for a well-correlated and anti-correlated wind regime 545 are shown in Figure 25. 546



548

549 550 Figure 25: Net load curve for a wind regime that is well-correlated with the demand profile versus a wind regime that is anti-correlated with the demand profile

Figure 26 shows wind regimes that are well-correlated with the demand profile (top) and anticorrelated with the demand profile (middle). Averaged over the entire year, integrating an anticorrelated wind regime results in a 35% increase in curtailment, 24% increase in demand response utilization, 4% increase in cost, and 7% increase in marginal cost variability compared to integrating a well-correlated regime.

556

557 Storage utilization draws down the curtailment resulting from integrating an anti-correlated 558 wind resource, as shown on the bottom portion of Figure 26. Adding a storage asset to a system 559 integrating a wind regime that is anti-correlated with demand reduces curtailment by 14% and

560 demand response utilization by 12%.



Figure 26: Generation by technology type for an example week integrating a wind resource that is well-correlated with the demand profile (top), anti-correlated with the demand profile (middle), and anti-correlated with demand but includes both demand response and storage (bottom)

### 569 4.4 The impact of geographic coincidence factors on integration requirements

570 Deploying two well-correlated wind regimes (with mirroring output), or two anti-correlated

571 wind regimes (with complementing output), has a large impact on integration requirements. As

572 shown in Figure 27, deploying two anti-correlated wind regimes results in smaller extreme

573 negative or positive net loads. These negative net loads result in VRE curtailment that can only
574 be mitigated with storage utilization, but not with increased system flexibility. The smaller

- 575 negative net loads in the anti-correlated set will necessitate less storage utilization to achieve
- the same amount of curtailment, as well as less generation from non-VRE assets due to the
- 577 smaller positive net loads.



578 579

Figure 27: Net load curve of two well-correlated and anti-correlated wind regimes

580 The curtailment increases from 5 GWh for an anti-correlated pair to 4,127 GWh for a well-581 correlated pair. Additionally, the well-correlated pair utilizes over 5 times as much storage, 582 exhibits a 47% increase in average system cost, and an 69% increase in GHG emissions over the 583 case of integrating two anti-correlated sites. On the other hand, increasing the number of wind 584 regimes in a system has a much smaller impact on integration requirements as compared to 585 integrating anti-correlated sets of wind regimes).

## **4.5** The impact of inter-resource correlation factor on integration

### 587 requirements

588 Analogous to deploying two complementary wind regimes, deploying complementary wind and 589 solar regimes results in smaller extreme negative or positive net loads, as shown in Figure 28.



590 591

593 The larger negative net loads in the well-correlated set require more storage deployment to offset the curtailment that would otherwise occur. The well-correlated wind and solar set incurs 594 595 almost 180% more wind curtailment, over 800% more solar curtailment, and 50% more storage utilization as compared to the scenario integrating two anti-correlated sets. An example week 596

- 597 demonstrating the difference between integrating a well-correlated and anti-correlated wind-
- 598 solar pair is shown in Figure 29.
- 599



602 603

(bottom) wind and solar pair

Additionally, integrating a well-correlated wind and solar regime incurs a 20% increase in
 average cost, 37% increase in marginal cost variability, 15% increase in GHG emissions, and 19%
 increase in non-VRE ramping events.

607 **5 Discussion** 

### 608 5.1 Relative impact of alternative integration strategies

The overall impact associated with integrating VRE regimes on the grid differs depending on the integration scenario. Decreasing the system's non-VRE flexibility factor increases the cumulative integration costs most significantly, as measured by average marginal cost (100%), GHG

612 emissions (100%), VRE curtailment (100%), and storage and DR asset utilization (90%).

613 Integrating a regime that is anti-correlated with the demand profile, charging curtailment costs,

and integrating a highly variable VRE regime, also increase integration costs, but to a lesser

extent. On the other hand, integrating an anti-correlated pair of wind regimes incurs the least

616 integration requirements, as measured by average marginal cost (almost 40% of relative

617 impact), GHG emissions (20%), VRE curtailment (<0.05%), and storage and DR utilization (3%). In

618 terms of VRE integration requirements, this scenario is followed by integrating an anti-

619 correlated wind and solar pair. Deploying two anti-correlated wind pairs is a better strategy than

620 deploying an anti-correlated wind-solar pair. The most effective balancing strategy that does

not require multi-project coordination is to deploy VRE resources with low hourly variability. The
 relative impact of VRE variability on different integration metrics is summarized in Figure 30.

623

624 The results from this analysis contribute to the growing discussion on the impacts of VRE 625 integration. Denholm and Hand provided one of the early VRE integration impact assessments 626 by quantifying the curtailment and relative VRE costs of electricity systems with increasing VRE 627 penetrations (Denholm & Hand, 2011). They highlight the significant impact of the system's 628 flexibility factor on VRE integration metrics (Denholm & Hand, 2011), which is a key factor in this 629 analysis as well. More specifically, Denholm and Hand find that achieving 80% VRE penetration 630 necessitates eliminating baseload "must-run" generation and addressing the mismatch between 631 VRE supply and electricity demand (Denholm & Hand, 2011). Additionally, Frew et al. determine 632 the impacts of integrating four flexibility mechanisms in high VRE penetration scenarios: 633 geographic aggregation, renewable overgeneration, storage, and flexible load (Frew, Becker, 634 Dvorak, Andresen, & Jacobson, 2016). From a cost perspective, Frew et al. find that geographic 635 aggregation has the greatest system benefit (Frew et al., 2016). Like Denholm and Hand, Frew et 636 al. highlight the need for flexible load as VRE penetration increases to increase asset utilization rates and decrease system levelized costs (Frew et al., 2016). Kondziella and Bruckner synthesize 637 638 recent analyses of flexibility requirements for high-VRE penetration (Kondziella & Bruckner, 639 2016). Their results show the wide range for flexibility demand at differing VRE penetrations; for 640 example at 80% VRE penetration, demand for flexibility ranges from 40 -120 GW for the German power sector (Kondziella & Bruckner, 2016). This wide range reflects the range of assumptions 641 642 that impact VRE integration metrics. Analyses of VRE integration in South America are less 643 common. Schmidt et al. optimize the portfolio of hydro, wind and solar PV in Brazil to minimize 644 thermal power production and its associated GHG emissions (Schmidt et al., 2016). Using a daily 645 dispatch model Schmidt et al. find that existing hydropower capacity can balance the variability 646 from a 46% penetration of renewable electricity, assuming access to 24 hours of electricity 647 storage, adequate transmission expansions, and land availability (Schmidt et al., 2016). The 648 analysis in the present paper contributes to this VRE integration discussion, through a greater 649 understanding of the implications of distinct VRE resource typologies. By developing VRE 650 characterization metrics in the context of integration analyses, the current analysis provides a 651 new perspective on VRE integration impact analysis which could improve electricity system

652 planning activities.



Figure 30: Relative impact of VRE variability on different integration strategies (hourly scale)

#### 5.2 Limitations of the analysis 658

This analysis embodies numerous approximations and assumptions. There are limitations in the 659

660 MERRA dataset itself: the assimilation data are imperfect, the large spatial resolution of data

661 masks local variations in resource quality, and the hourly temporal resolution occludes sub-

- hourly variability; variability at the millisecond, second, and minutes scale has been analyzed by 662
- (Makarov et al., 2009) (Parsons et al., 2006) and (Smith, Milligan, DeMeo, & Parsons, 2007). The 663

664 methodology used to select specific wind and solar grid points is simplistic, only considering the 665 average resource value, and thus ignoring important factors such as proximity to transmission 666 infrastructure, construction suitability, or access to transport networks. Additionally, the VRE 667 power models inevitably embody sources of error. The variability metrics entail limitations 668 associated with their highly aggregated formulations. While this aggregation enables 669 visualization of overall trends, extreme but infrequent events are averaged out. Additionally, the 670 block-form demand profile used for the DR metric includes historical data from only one South 671 American electricity system (Chile), and remains constant throughout the 35-year analysis 672 period. Finally, the UC model employs assumptions which may lack accuracy by assuming 673 generalized generator characteristics. VRE regimes deployed in the UC were chosen to highlight 674 the impact of different VRE characterizations, are not necessarily representative of 'realistic' 675 VRE projects.

### 676 6 Conclusions

677 This paper proposes a methodology for characterizing variable renewable energy sources in 678 terms of the balancing strategies that can be employed to integrate them into the existing 679 electrical system. The methodology epitomizes the tradeoff between maximizing widespread 680 relevancy, while maintaining sufficient accuracy; the goal is to develop an integrated framework 681 that can provide a suitable high level perspective for planners during a proposed electricity 682 system transition. Variability on an hourly basis is quantified based on the frequency and 683 magnitude of hourly ramp events, with relevance to flexibility resources with hourly 684 dispatchability and reservoir size. Weekly-to-seasonal variability is characterized using relative 685 frequency distributions. Inter-annual variability is quantified using the annual average resource 686 over the 35-year period, informing long term backup or storage infrastructure requirements. 687 The correlation between the VRE resource and the demand profile is quantified by calculating 688 the average resource within distinct demand bands, informing the need for demand response 689 initiatives. Analogously, the correlation between wind and solar resource is quantified to inform 690 the value of interconnecting neighboring sites with transmission capacity. Finally, the 691 geographic coincidence function for increasingly large geographic areas informs the value of 692 expanding interconnections to increasingly large areas.

693

This characterization methodology is illustrated using South America and the results clearly
identify the most prevalent VRE regimes. The results illustrate the relationships between
different categories of balancing options. Approximately half of the wind grid points fit into one
of nine types with varying degrees of requirements in each balancing category. The two most
prevalent wind types are also the most demanding in terms of balancing requirements. Yet,
significantly, as much as 10% of the South American wind regimes appear to need little
investment in the form of balancing infrastructure.

701

System-level planning is the most important integration strategy. Strategic resource planning, by
 deploying anti-correlated wind-wind or wind-solar pairs, and strategic system planning, by
 designing high-flexibility-factor systems, are the two most effective strategies to mitigate VRE
 integration costs.

706

The goal of this characterization is to contribute to the set of tools that electricity system

708 planners can leverage when planning high VRE penetrations. Local planners can apply these

- tools to quantify the requirements for balancing resources, given different combinations of wind
- 710 and solar types.

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715

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- Development of VRE characterization metrics according to integration requirements
- Application of characterization metrics in a unit commitment dispatch model
- Evaluation of VRE resources according to integration requirements
- Flexibility and strategic resource aggregation minimize integration requirements